



FROELICH
ENGINEERS

Land Use Stormwater Drainage Report

Springdale Fire Station Improvements

31727 East Historic Columbia River Highway; Troutdale, OR 97019

For

Corbett Fire District

Regular maintenance and inspection are required on all components of the stormwater system. This plan provides instructions on how to maintain and inspect the system.

Prepared by: Evan Eykelbosch, PE
Froelich Engineers
17700 SW Upper Boones Ferry Rd, Suite 115
Portland, OR 97224
Froelich Project Number: 23-C021
Date: July 18, 2025

Land Use Stormwater Drainage Report

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I. Project Overview and Description

Existing Conditions

The existing site is located at 31727 East Historic Columbia River Highway (See Appendix A: Vicinity Map). The site is partially developed with a single fire truck garage and parking lot on the southern end of the site and a large undeveloped grass field on the northern half of the site. A retaining wall and a sloped hillside separate the north and south ends of the site. The site drains to the south. Along the southern property line is the East Historic Columbia River Highway, owned by ODOT. Within the street is a public stormwater system. This stormwater main crosses the road just west of our site and discharges into Springdale Creek.

Proposed Conditions

The proposed development includes a new fire truck garage and parking lot. A new retaining wall will be constructed that pushes into the hillside to create sufficient space for the development of the site. Site improvements will include new concrete, asphalt, gravel and landscaped surfaces. In addition, some areas of existing impervious surface are being removed, resulting in a net reduction of impervious area when comparing existing conditions and proposed conditions. See Table 1 and Appendix B: Basin Maps.

II. Methodology

Stormwater Requirements

Multnomah County is the jurisdiction with authority over the stormwater requirements for this site. Per Multnomah County Zone Code Section 39.4575(F)(2), "Stormwater /drainage control systems are required for new impervious surfaces greater than 500 square feet in area. The system shall be adequate to ensure that the rate of runoff from the lot for 10 year 24-hour storm event is not greater than that before the development." Our understanding is that this refers to the increase in total impervious area of the site. Therefore, because the site has a net reduction of the impervious area between the existing condition and the proposed conditions, no stormwater management requirements (treatment or detention) are triggered. The project will provide conveyance for the new impervious areas as well as some of the existing areas.

Due to the stormwater system being located within the ODOT right-of-way, ODOT has additional detention requirements for the site. ODOT requires the post-development 50-year storm peak runoff not exceed the existing 50-year storm peak runoff. Because the site has a net decrease in the impervious area, this site meets the runoff requirements. (See Table 2 & 3 below)

Proposed Stormwater System

The proposed development will include a new fire truck garage, a courtyard, a paved service/parking area, and a graveled service/parking area. These areas will be collected within a series of area drains and downspouts. The runoff will be conveyed into a system of stormwater pipes, which will be routed into a public catch basin located along the East Historic Columbia River Highway. The site improvements are limited to Basin B. Runoff from "Subbasin B-1" is collected and conveyed through a buried 4" diameter stormwater pipe. Runoff from "Subbasin B-2" surface flows south toward the street (See Appendix B: Basin Areas). The total impervious area runoff decreases; therefore, there are no treatment or detention requirements. See Appendix F: Utility Plan/Details.

Stormwater conveyance is designed to accommodate the 50-year stormwater event. See Appendix D: Conveyance Calculations and Appendix B: Basin Areas for the indicated subbasins.

Land Use Stormwater Drainage Report

Columbia West completed infiltration testing, and it was determined that, due to high groundwater and poor infiltration, infiltration for disposal would not be acceptable on this site. See Appendix E: Geotechnical Report.

III. Analysis

Table 1a:
Existing Conditions

Basins	Pervious		Impervious		total		Flow Q (50yr)
	sf	ac	sf	ac	sf	ac	cfs
Basin A	11,576	0.266	400	0.009	11,976	0.275	0.20
Basin B	476	0.011	7,948	0.182	8,424	0.193	0.22
total =	12,052		8,348		20,400		0.42

Table 1b:
Proposed Conditions

Basins	Pervious		Impervious		total		Flow Q (50yr)
	sf	ac	sf	ac	sf	ac	cfs
Basin A	9,307	0.214	0	0.000	9,307	0.214	0.15
Basin B	3,116	0.072	7,977	0.183	11,093	0.255	0.26
total =	12,423		7,977		20,400		0.41

Table 2:
Stormwater Flow Rate Table

Sub-Basins	Pervious		Impervious		total		Flow Q (50yr)
	sf	ac	sf	ac	sf	ac	cfs
SubBasin B-1	1,832	0.042	3,444	0.079	5,276	0.121	0.12
SubBasin B-2	1,284	0.029	4,533	0.104	5,817	0.134	0.14

Table 3: Stormwater Conveyance

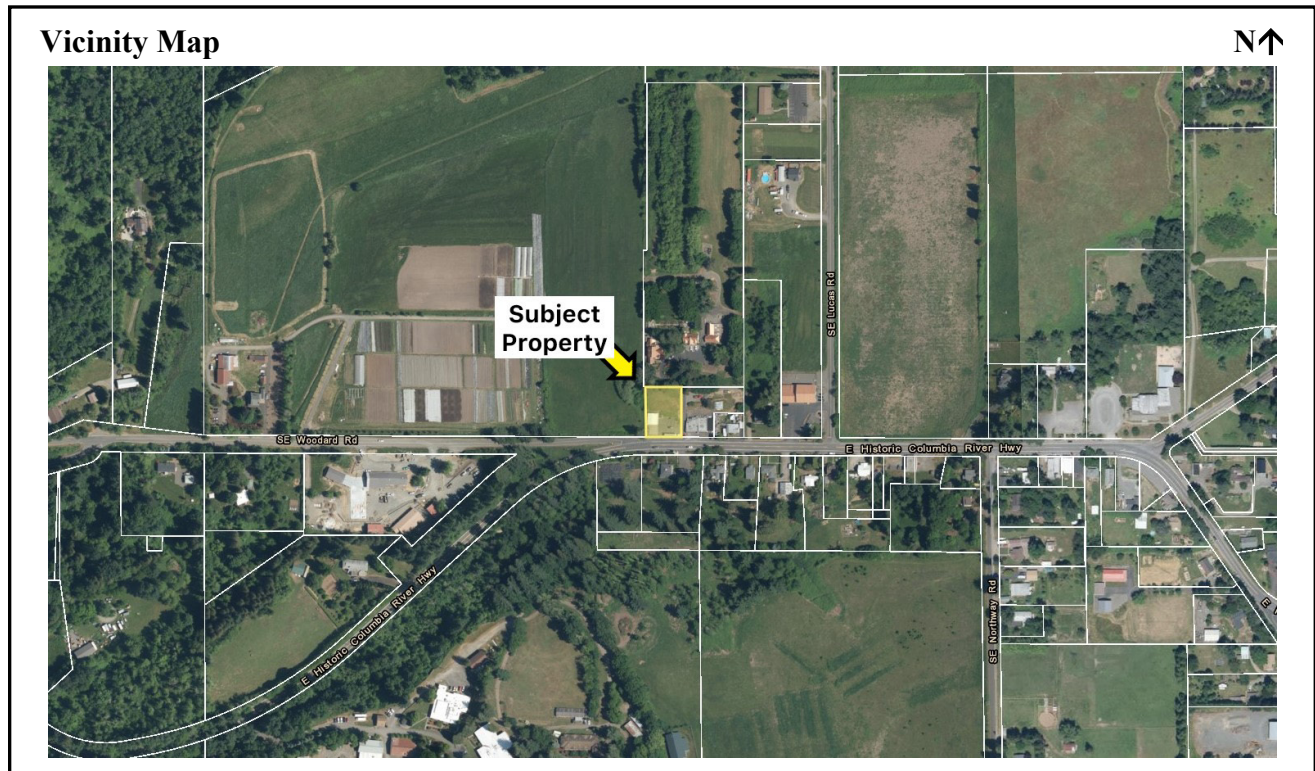
Peak Flow Rate (cfs) for a 24-hour Storm Event	
50-yr Existing	50-yr Proposed
0.42 cfs	0.41 cfs

IV. Engineering Conclusion

The proposed design meets and exceeds the requirements for stormwater management set forth by Multnomah County.

V. Appendices

Land Use Stormwater Drainage Report

Appendix A: Vicinity Map

Appendix B: Basin Maps

SPRINGDALE FIRE STATION IMPROVEMENTS

31727 EAST HISTORIC COLUMBIA RIVER HWY
TROUTDALE, OR, 97019

LAND USE
SET

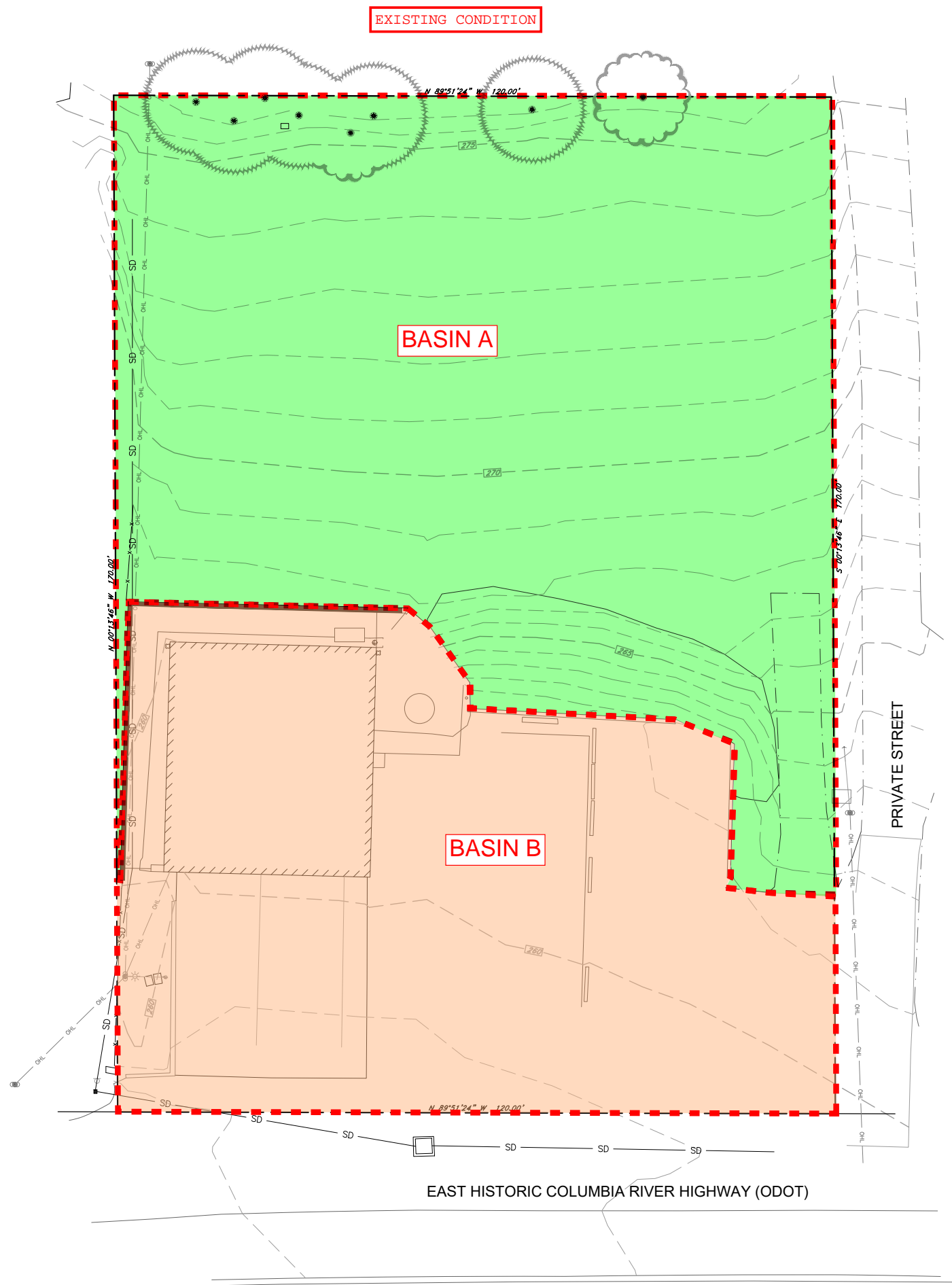
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PROJECT MANAGER:		EMERSON
DESIGNER:		EMERSON
DRAWN BY:		EYKELBOSCH
PROJECT NO:		----
DATE:		10/11/24
SCALE:		AS SHOWN

SHEET TITLE:
EXISTING
CONDITIONS

SHEET NUMBER:

C1.01

LAND USE SET





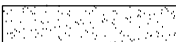

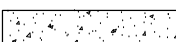



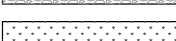
31727 EAST HISTORIC COLUMBIA RIVER HWY
 BOULDER CO 80504

REV	DATE	ISSUE TITLE
PROJECT MANAGER:		EMERSON
DESIGNER:		EMERSON
DRAWN BY:		EYKELBOSCH
PROJECT NO:		----
DATE:		10/11/24
SCALE:		AS SHOWN

SHEET NUMBER:

AND USE SET



	PROPERTY LINE	
	CONCRETE SIDEWALK	
	STANDARD ASPHALT PAVEMENT	
	HEAVY CONCRETE	
	GRAVEL	
	LANDSCAPING (BY OTHERS)	

Plotted: 7/14/25 at 2:27pm By: atomlinson

31727 EAST HISTORIC COLUMBIA RIVER HWY
 BOULDER CO 80501

REV	DATE	ISSUE TITLE
PROJECT MANAGER:		EMERSON
DESIGNER:		EMERSON
DRAWN BY:		ATOMLINSON
PROJECT NO:		-----
DATE:		10/11/24
SCALE:		AS SHOWN

SHEET NUMBER:

LAND USE SET



SCALE 1 INCH = 10 FEET

A horizontal scale bar with alternating black and white segments. Below the bar, the numbers 10, 0, and 10 are printed, indicating distances in feet. The total length of the bar represents 20 feet.

Appendix C: Assumptions



Assumptions

Springdale Fire Station Improvements
Project #23-C021

Santa Barbara Unit Hydrograph (SBUH) Assumptions:

(used for Water Quality, Flow Control, Conveyance)

Water Quality (WQ) Storm Event =	1.5 in/24-hours per ODOT Hydraulics Manual
2-year Storm Event=	3.0 in/24-hours per ODOT Hydraulics Manual
10-year Storm Event=	4.0 in/24-hours per ODOT Hydraulics Manual
50-year Storm Event=	5.0 in/24-hours per ODOT Hydraulics Manual

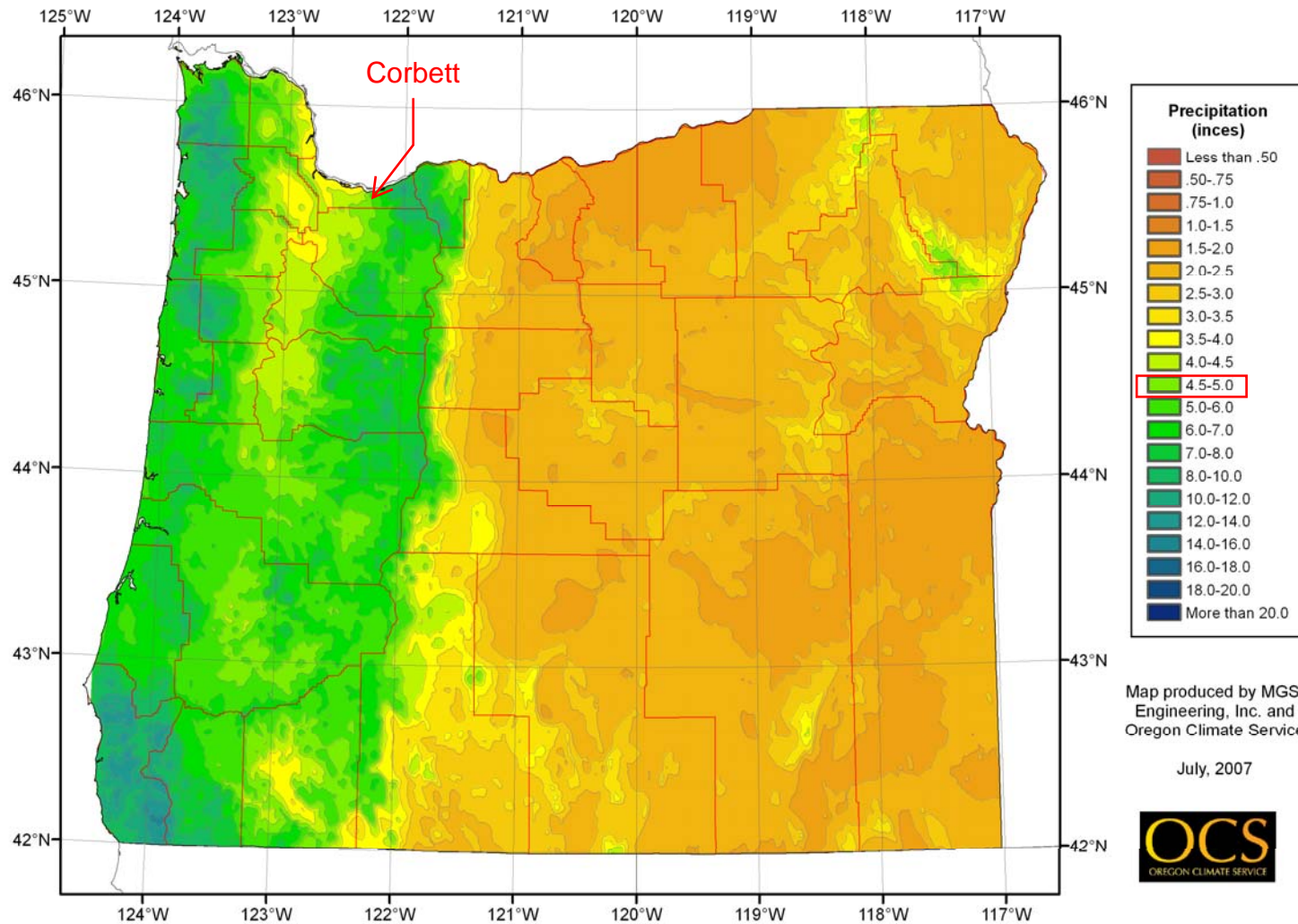
Time of Concentration **5.0** minutes

Roughness Coefficient **0.013**

Curve Number Assumptions:

Impervious Area =	98	
Pervious Area =	81	Pre-Developed

24-hour 50-year Precipitation, Oregon



Appendix D: Conveyance Calculations



Basin Areas

Springdale Fire Station Improvements
Project #23-C021

Existing Conditions

<u>Basins</u>	<u>Pervious</u>		<u>Impervious</u>		<u>total</u>		<u>Flow Q (50yr)</u>
	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>cfs</u>
Basin A	11,576	0.266	400	0.009	11,976	0.275	0.20
Basin B	476	0.011	7,948	0.182	8,424	0.193	0.22
total =	12,052		8,348		20,400		

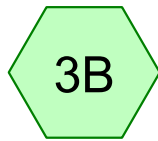
Proposed Conditions

<u>Basins</u>	<u>Pervious</u>		<u>Impervious</u>		<u>total</u>		<u>Flow Q (50yr)</u>
	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>cfs</u>
Basin A	9,307	0.214	0	0.000	9,307	0.214	0.15
Basin B	3,116	0.072	7,977	0.183	11,093	0.255	0.26
total =	12,423		7,977		20,400		

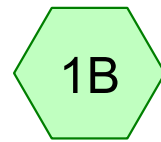
<u>Sub-Basins</u>	<u>Pervious</u>		<u>Impervious</u>		<u>total</u>		<u>Flow Q (50yr)</u>
	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>sf</u>	<u>ac</u>	<u>cfs</u>
SubBasin B-1	1,832	0.042	3,444	0.079	5,276	0.121	0.12
SubBasin B-2	1,284	0.029	4,533	0.104	5,817	0.134	0.14



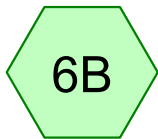
Subbasin B-1



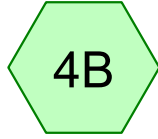
Basin A



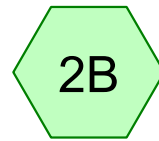
Basin A



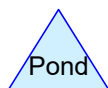
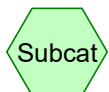
Subbasin B-2



Basin B



Basin B



Routing Diagram for 23-C021_HydroCAD

Prepared by Froelich Engineers, Printed 7/17/2025

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23-C021_HydroCAD

Prepared by Froelich Engineers

Printed 7/17/2025

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	50-Year	Type IA 24-hr		Default	24.00	1	5.00	2

23-C021_HydroCAD

Prepared by Froelich Engineers

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Type IA 24-hr 50-Year Rainfall=5.00"

Printed 7/17/2025

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Time span=0.04-36.00 hrs, dt=0.20 hrs, 181 points

Runoff by SBUH method, Weighted-Q

Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment1B: Basin A	Runoff Area=11,976 sf 3.34% Impervious Runoff Depth=3.05" Tc=5.0 min CN=WQ Runoff=0.20 cfs 3,039 cf
Subcatchment2B: Basin B	Runoff Area=8,424 sf 94.35% Impervious Runoff Depth>4.66" Tc=5.0 min CN=WQ Runoff=0.22 cfs 3,274 cf
Subcatchment3B: Basin A	Runoff Area=9,307 sf 0.00% Impervious Runoff Depth=2.99" Tc=5.0 min CN=81 Runoff=0.15 cfs 2,316 cf
Subcatchment4B: Basin B	Runoff Area=11,093 sf 71.91% Impervious Runoff Depth>4.26" Tc=5.0 min CN=WQ Runoff=0.26 cfs 3,942 cf
Subcatchment5B: Subbasin B-1	Runoff Area=5,276 sf 65.28% Impervious Runoff Depth>4.15" Tc=5.0 min CN=WQ Runoff=0.12 cfs 1,823 cf
Subcatchment6B: Subbasin B-2	Runoff Area=5,817 sf 77.93% Impervious Runoff Depth>4.37" Tc=5.0 min CN=WQ Runoff=0.14 cfs 2,119 cf

Total Runoff Area = 51,893 sf Runoff Volume = 16,512 cf Average Runoff Depth = 3.82"
53.17% Pervious = 27,591 sf 46.83% Impervious = 24,302 sf

23-C021_HydroCAD

Prepared by Froelich Engineers

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Type IA 24-hr 50-Year Rainfall=5.00"

Printed 7/17/2025

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Summary for Subcatchment 1B: Basin A

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.20 cfs @ 8.00 hrs, Volume= 3,039 cf, Depth= 3.05"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt= 0.20$ hrs

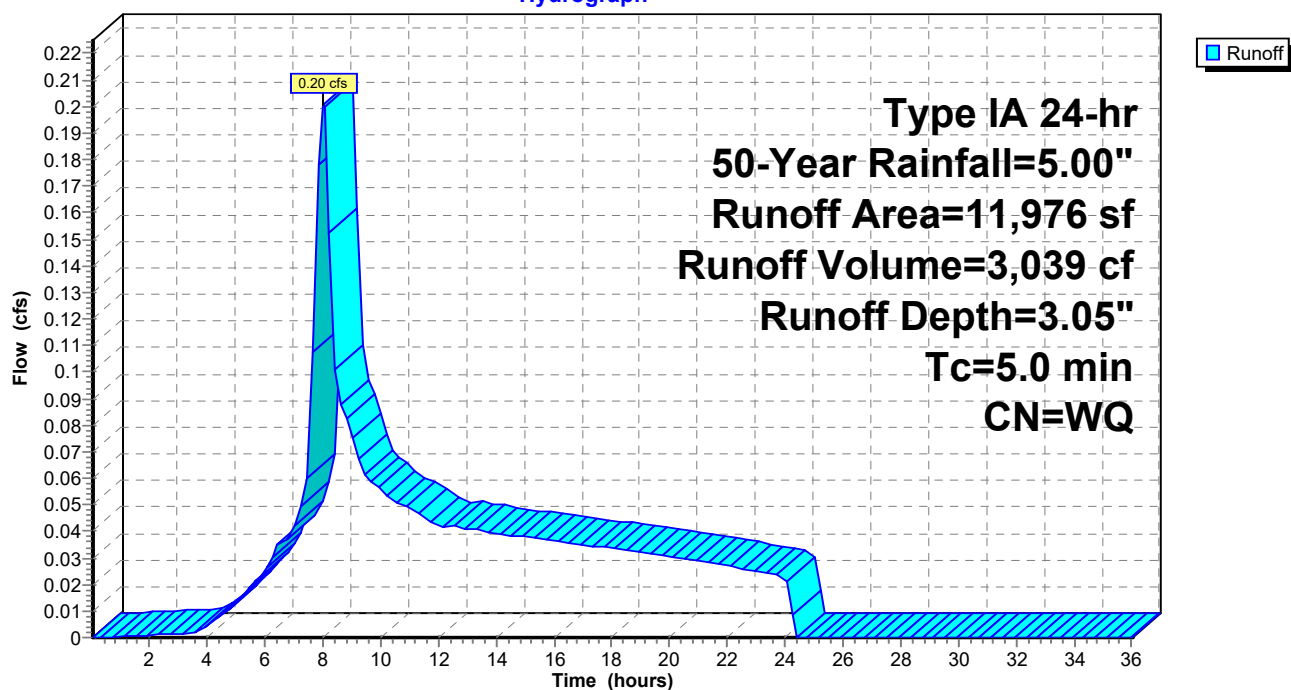
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	11,576	81	
*	400	98	
	11,976		Weighted Average
	11,576	81	96.66% Pervious Area
	400	98	3.34% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 1B: Basin A

Hydrograph



23-C021_HydroCAD

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Type IA 24-hr 50-Year Rainfall=5.00"

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Summary for Subcatchment 2B: Basin B

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.22 cfs @ 7.97 hrs, Volume= 3,274 cf, Depth> 4.66"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt=0.20$ hrs

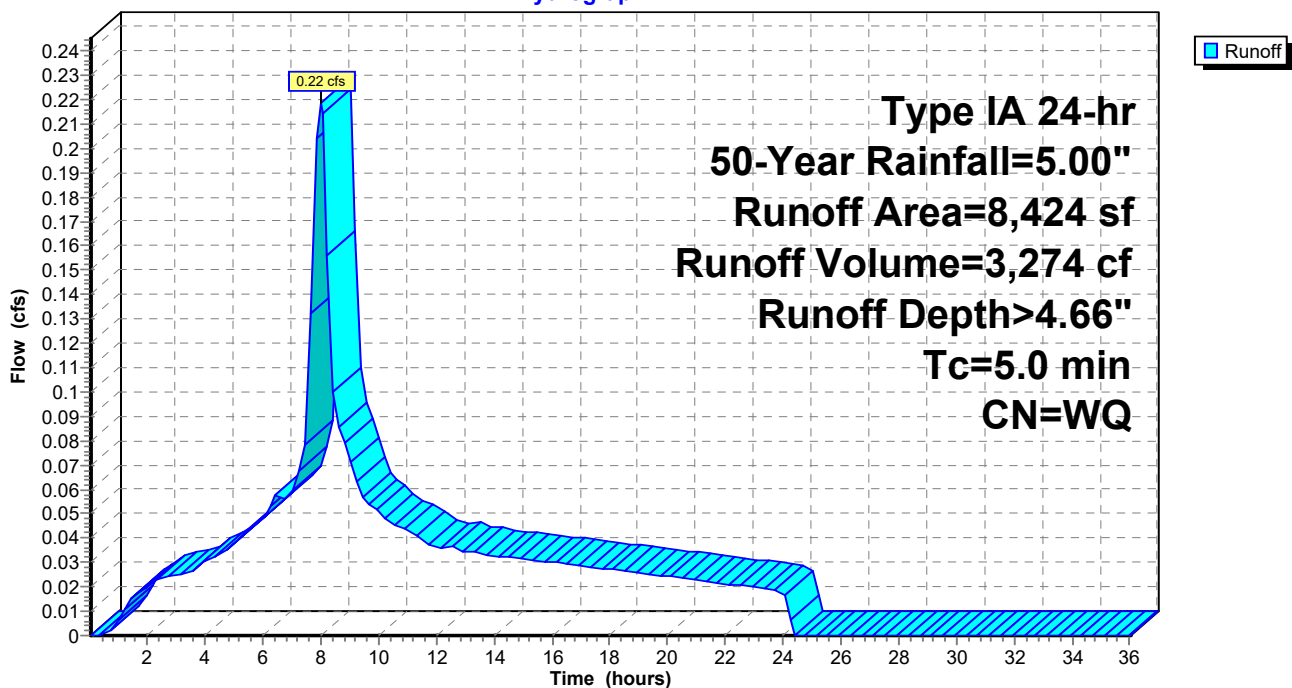
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	476	81	
*	7,948	98	
<hr/>			
	8,424		Weighted Average
	476	81	5.65% Pervious Area
	7,948	98	94.35% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 2B: Basin B

Hydrograph



23-C021_HydroCAD

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Type IA 24-hr 50-Year Rainfall=5.00"

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Summary for Subcatchment 3B: Basin A

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.15 cfs @ 8.00 hrs, Volume= 2,316 cf, Depth= 2.99"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt= 0.20$ hrs

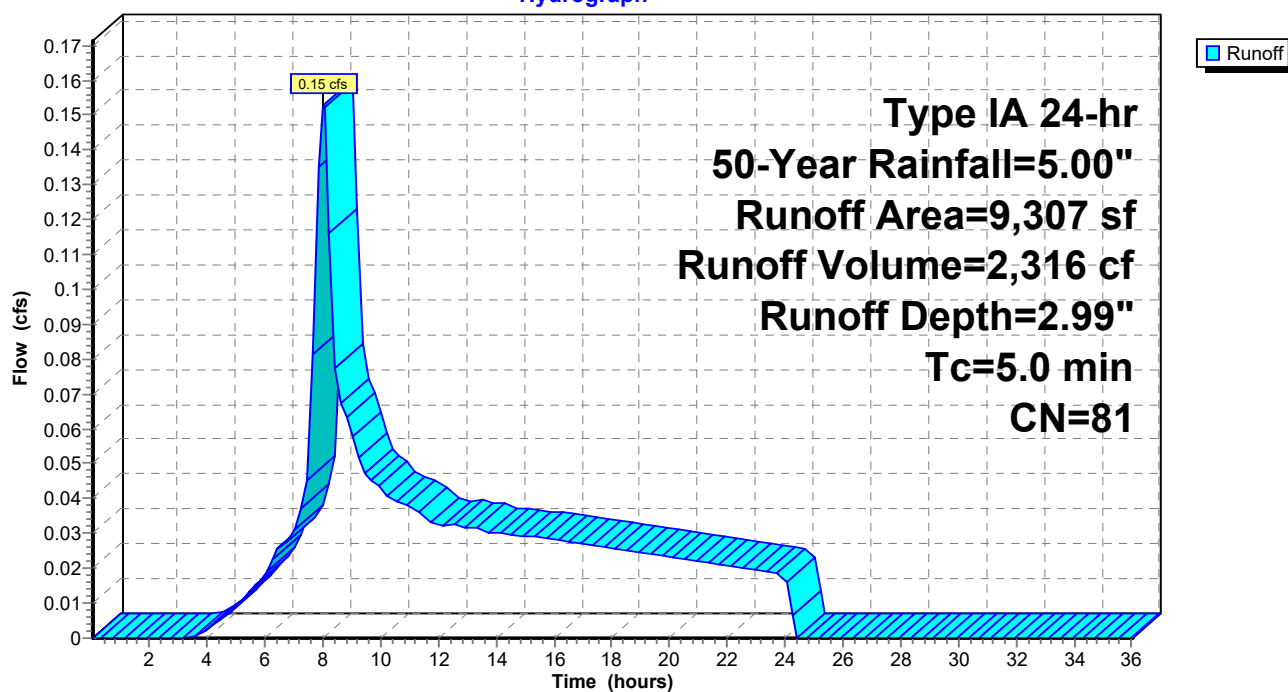
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	9,307	81	
	9,307	81	100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 3B: Basin A

Hydrograph



23-C021_HydroCAD

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Type IA 24-hr 50-Year Rainfall=5.00"

Printed 7/17/2025

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Summary for Subcatchment 4B: Basin B

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.26 cfs @ 7.98 hrs, Volume= 3,942 cf, Depth> 4.26"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt= 0.20$ hrs

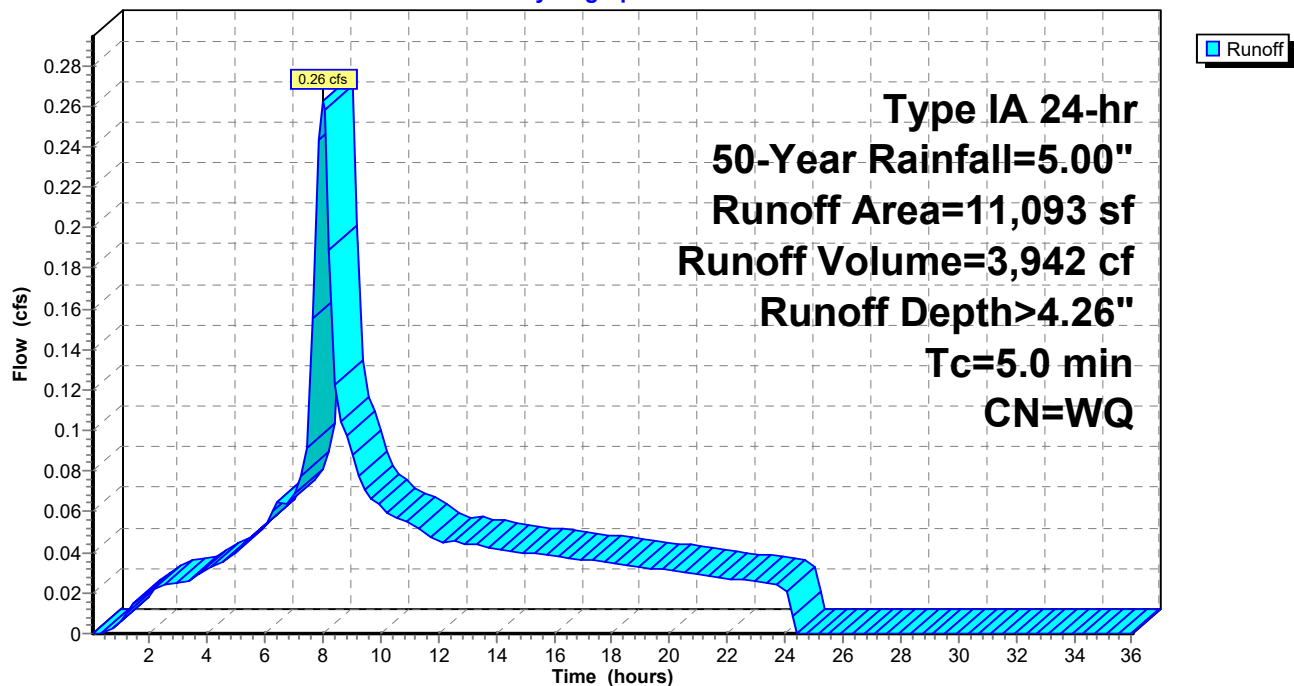
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	3,116	81	
*	7,977	98	
	11,093		Weighted Average
	3,116	81	28.09% Pervious Area
	7,977	98	71.91% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 4B: Basin B

Hydrograph



Summary for Subcatchment 5B: Subbasin B-1[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.12 cfs @ 7.98 hrs, Volume= 1,823 cf, Depth> 4.15"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt=0.20$ hrs

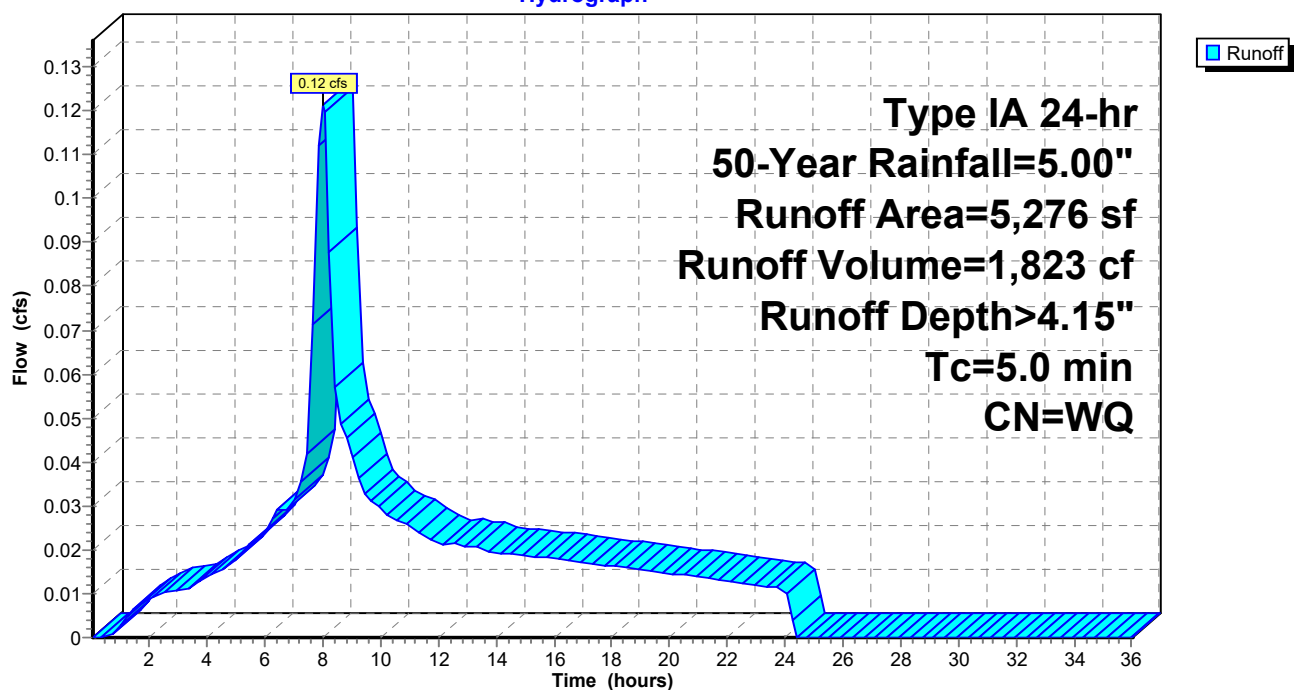
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	1,832	81	
*	3,444	98	
	5,276		Weighted Average
	1,832	81	34.72% Pervious Area
	3,444	98	65.28% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment 5B: Subbasin B-1

Hydrograph



23-C021_HydroCAD

Prepared by Froelich Engineers

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Type IA 24-hr 50-Year Rainfall=5.00"

Printed 7/17/2025

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Summary for Subcatchment 6B: Subbasin B-2

[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.14 cfs @ 7.97 hrs, Volume= 2,119 cf, Depth> 4.37"

Runoff by SBUH method, Weighted-Q, Time Span= 0.04-36.04 hrs, $dt= 0.20$ hrs

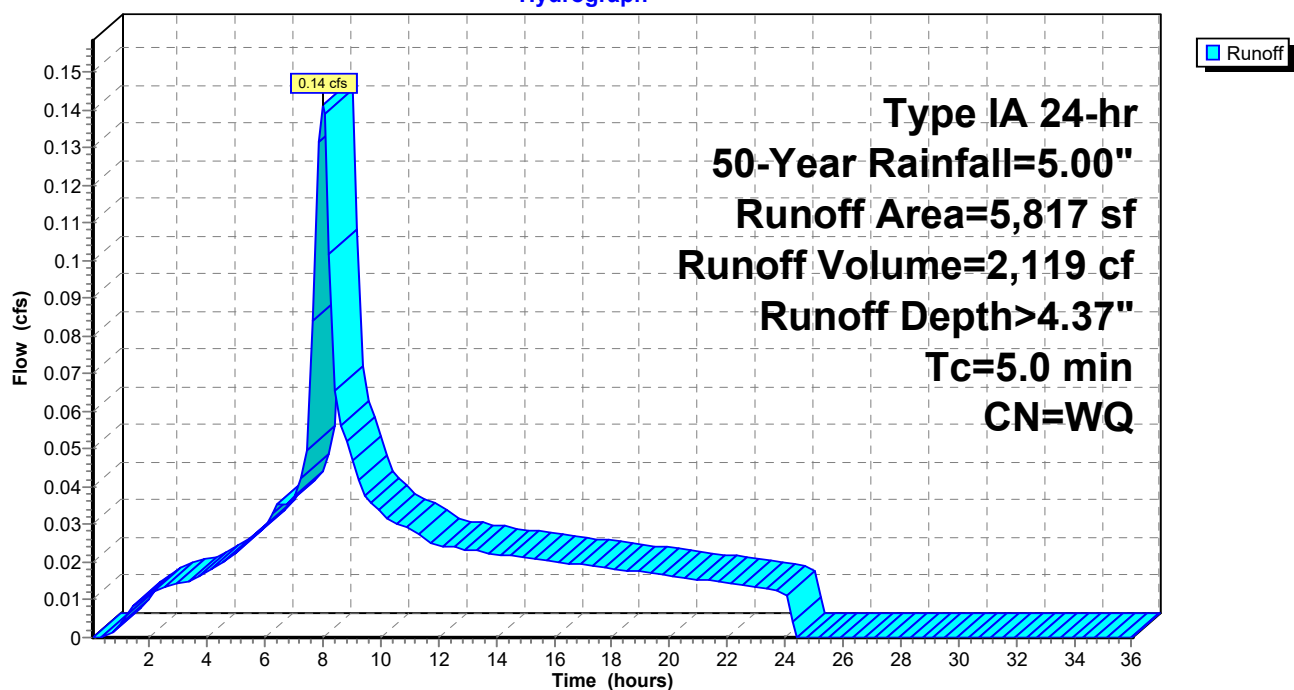
Type IA 24-hr 50-Year Rainfall=5.00"

	Area (sf)	CN	Description
*	1,284	81	
*	4,533	98	
	5,817		Weighted Average
	1,284	81	22.07% Pervious Area
	4,533	98	77.93% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

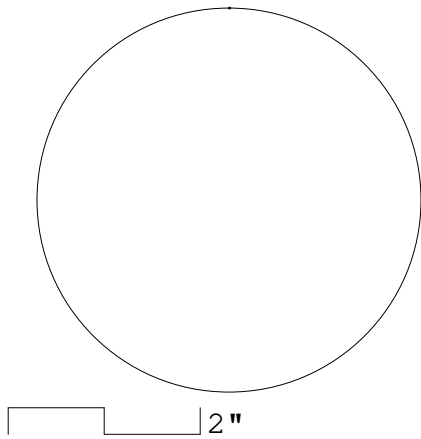
Subcatchment 6B: Subbasin B-2

Hydrograph



Project 23-C012
Springdale Fire Station Improvements

GRAVITY PIPE FLOW (Chezy-Manning)
4-inch Pipe @ 1%



diameter = 4.0"
slope = 1.00%
material: ABS, PVC
Manning's n = 0.013
depth of flow = 100.00% of diameter (full)

wetted perimeter = 1.05'
area = 0.09 s.f.
hydraulic radius = 0.08'
velocity = 2.18 fps
flow = 0.19 cfs

Appendix E: Geotechnical Report

**Report of Geotechnical
Engineering Services**

Springdale Station

Troutdale, Oregon

March 29, 2024

Geotechnical ■ Environmental ■ Special Inspections

Columbia West
Engineering, Inc



March 29, 2024

Corbett Fire District #14
36930 Historic Columbia River Highway
Corbett, OR 97019

Attn: Dave Flood

**Re: Report of Geotechnical Engineering Services
Springdale Station
31727 Historic Columbia River Highway
Troutdale, Oregon
CWE Project: CFD-1-01-1**

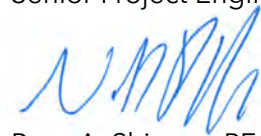
Columbia West Engineering, Inc. (Columbia West) is pleased to present this report of geotechnical engineering services for the Springdale Station project located in Troutdale, Oregon. Our services were conducted in accordance with our proposal dated January 23, 2024.

We appreciate the opportunity to work on the project. Please contact us if you have any questions regarding this document.

Sincerely,



Jason F. Merritt, PE
Senior Project Engineer



Signed for
Brett A. Shipton, PE, GE
Principal Engineer



cc: Erik Matthews, em architecture llc

JFM:NNP:kat

Attachments

Document ID: CFD-1-01-1-032924-geor.docx

EXECUTIVE SUMMARY

This executive summary presents the primary geotechnical considerations associated with the Springdale Station project located in Troutdale, Oregon. Our conclusions and recommendations are based on the subsurface information presented in the report and proposed development information provided by the design team. A detailed discussion of the geotechnical considerations summarized here is presented in respective sections of the report.

- The proposed structure can be supported on conventional spread footings bearing on firm, native soil or structural fill overlying firm, native soil.
- Based on the results of our site-specific seismic hazard evaluation, the parameters provided by ASCE 7-16 general response spectrum for Site Class C should be used for the site.
- Although not observed in the borings, undocumented fill may be present at the site, particularly below existing structural elements. All undocumented fill beneath proposed improvements should be assessed by Columbia West following demolition when subgrade conditions are exposed.
- Moisture conditioning will be likely be required to use the on-site soil as structural fill. Accordingly, extended dry weather will be required to adequately condition and place the silt as structural fill. It will be difficult, if not impossible, to adequately compact the on-site soil during the rainy season or during prolonged periods of rainfall.
- Based on results of in-situ infiltration testing in one of the borings, on-site stormwater infiltration systems are not feasible at the site.

3.3.2 Soil Conditions

3.3.2.1 Pavement Section

Borings B-1 and B-2 were drilled through a pavement section consisting of 5 inches of AC underlain by 6 inches of aggregate base.

3.3.2.2 Fine-Grained Alluvium

Silt with varying proportions of sand is present below the AC sections (B-1 and B-2) and in the south-facing slope (HA-1). The silt observed in the borings varies from medium stiff to stiff. Laboratory testing indicates the moisture content of native silt ranges from 29 to 38 percent and the fines content (percent passing the U.S. Standard No. 200 sieve) is between 53 and 95 percent. Atterberg limit testing indicates the silt has medium plasticity.

3.3.3 Groundwater

Perched groundwater was observed in borings B-1 and B-2 at depths of 3 and 3.5 feet BGS, respectively. Seeps were observed in boring HA-1 at a depth of approximately 4 feet below top of slope elevation and are likely from surface infiltration. The depth to perched groundwater may fluctuate in response to prolonged rainfall, seasonal changes, changes in surface topography, and other factors not observed during this study. Perched groundwater could be higher than observed in our explorations during the wet season or periods of persistent rainfall.

3.4 INFILTRATION TESTING

Infiltration testing was performed in boring B-2 at a depth of 2.5 feet BGS. Infiltration testing was conducted using the encased falling head method. Infiltration was not observed in the boring. Based on the results of our testing and observations, subsurface disposal of stormwater is not feasible in our opinion.

4.0 DESIGN

4.1 FOUNDATION SUPPORT

4.1.1 General

Provided foundation and floor slab loads are as described in Section 1.0 (Introduction) and the site is prepared as recommended in Section 5.0 (Construction), it is our opinion that the proposed building can be supported on conventional spread footings that bear on undisturbed, native soil or structural fill overlying undisturbed, native soil.

Foundations should not be supported on topsoil, tilled soil, undocumented fill, or loose/disturbed soil. If present below planned footings, these materials should be removed and replaced with structural fill as recommended in this report.

4.1.2 Bearing Capacity

Continuous perimeter wall and isolated spread footings should have minimum widths of 18 and 24 inches, respectively. The base of exterior footings should be at least 18 inches below the lowest adjacent exterior grade. The base of interior footings should bear at least 12 inches below the base of the floor.

Footings bearing on subgrade prepared as recommended in Section 5.1 (Site Preparation) should be sized based on an allowable bearing pressure of 2,500 psf. As the allowable bearing pressure



Appendix F: Utility Plan / Details

Appendix G: Operations and Maintenance

NOT INCLUDED WITH LAND USE